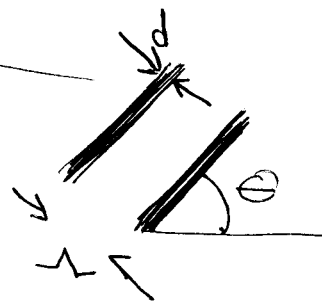
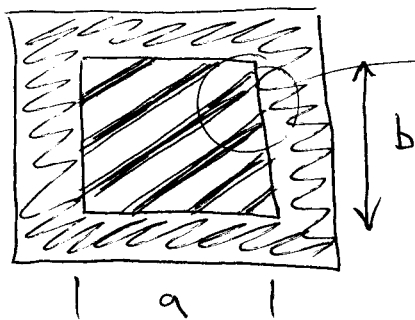
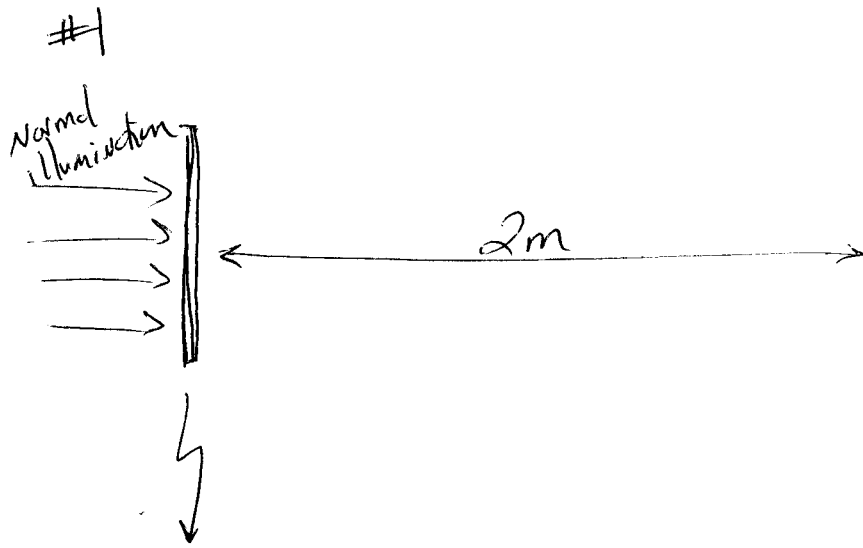
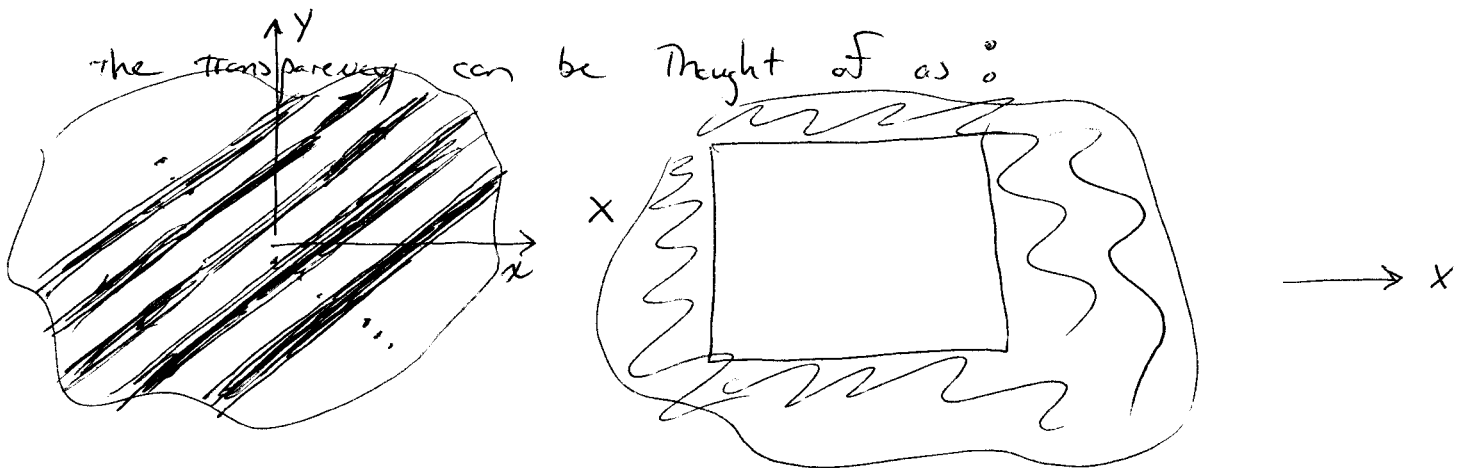


far field

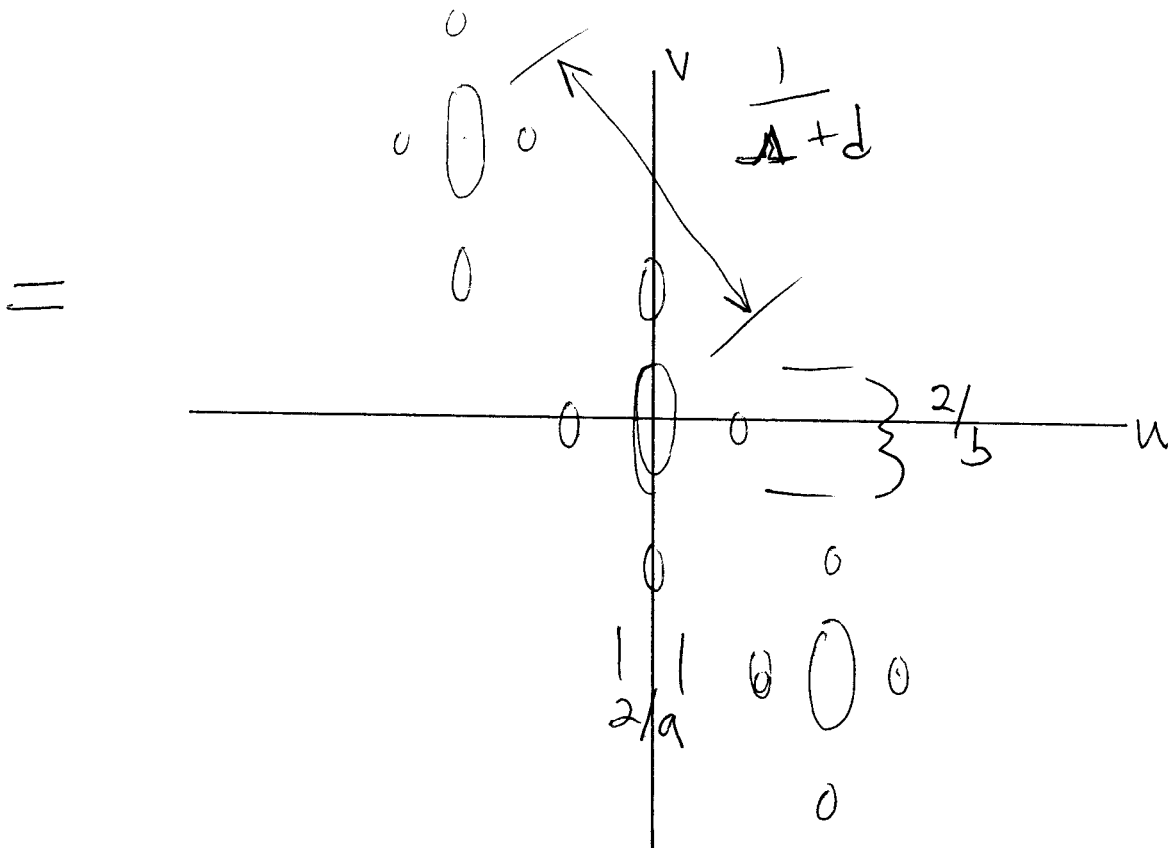
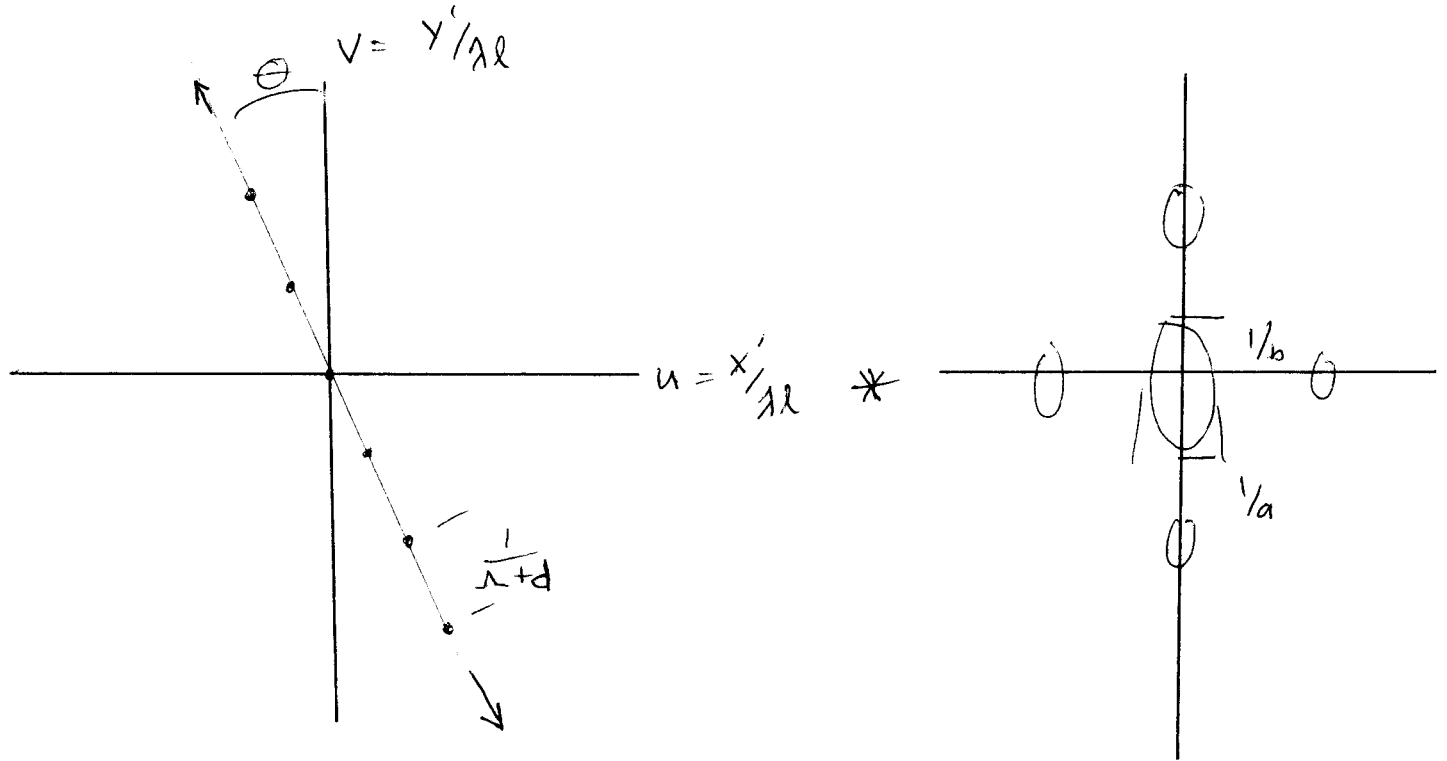


$$\begin{aligned} \lambda &= 10 \mu\text{m} \\ d &= 2 \mu\text{m} \\ \Theta &= 30^\circ \\ a \times b &= 5 \times 3 \text{ mm}^2 \\ l &= 2 \text{ m} \\ \lambda &= 0.5 \mu\text{m} \end{aligned}$$



i.e. multiplication in the spatial domain.

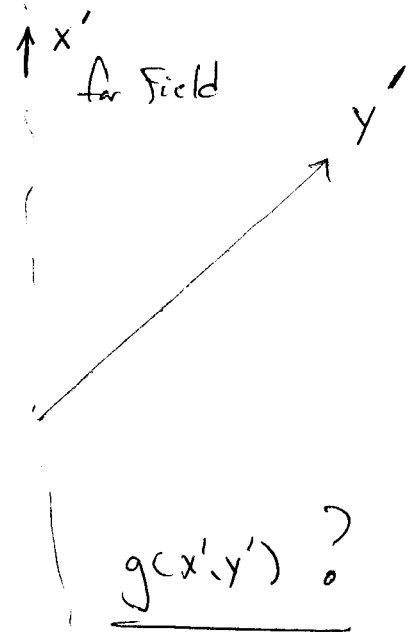
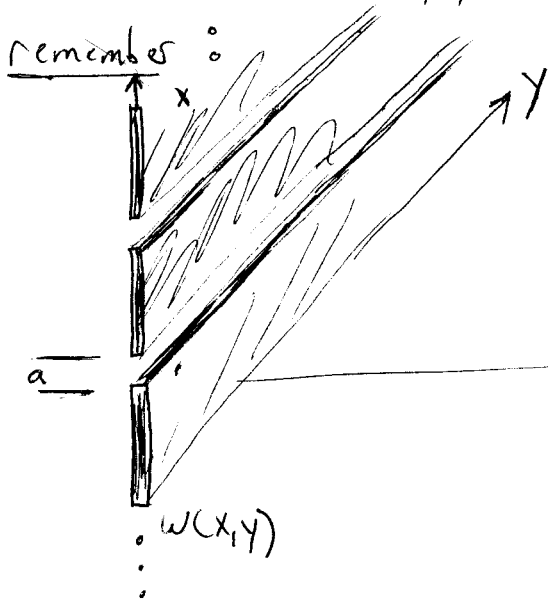
$\Leftrightarrow$ convolution in the freq domain. (Far field result)



for details see following
Pages.

Details : Note: This is much more math than you had to do. Simply drawing the end result was sufficient.

remember :



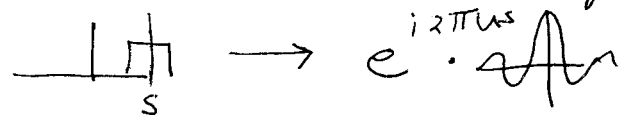
$$g(x', y')_{\text{far Field}} = \mathcal{FT}(w(x, y)) \Big|_{u = x'/\lambda l, v = y'/\lambda l}$$

$$W(u, v) = \int \underbrace{\sum_{j=1}^N \text{rect}\left(\frac{x - (j-1)\lambda}{a}\right)}_{= w(x, y)} e^{-i2\pi ux} dx$$

note : • a single rect's FT is the sinc



• a shifted function in the spatial domain is a modulation in frequency



so we have a bunch of ~~shifted~~ ^{modulated} summed sines

$$W(u, v) = \sum_{j=1}^N a \text{sinc}(a u) e^{i2\pi(j-1)\lambda u}$$

$$g(x', y') = \sum_{j=1}^N a \text{sinc}\left(a \frac{x'}{\lambda l}\right) e^{-i2\pi(j-1)\lambda \frac{x'}{\lambda l}}$$

$$g(x', y') = a \operatorname{sinc}\left(a \frac{x'}{\lambda l}\right) \sum_{j=1}^N e^{-i2\pi(j-1) \frac{\lambda x'}{\lambda l}}$$

$$= a \operatorname{sinc}\left(a \frac{x'}{\lambda l}\right) \sum_{j=1}^N e^{-i(j-1)\gamma}$$

$$\gamma = \frac{2\pi \lambda x'}{\lambda l}$$

$$= a \operatorname{sinc}\left(a \frac{x'}{\lambda l}\right) \sum_{j=0}^{N-1} (e^{-i\gamma})^j$$

Note:

$$\begin{aligned} \sum_{j=0}^{N-1} (e^{-i\gamma})^j &= \frac{1 - (e^{-i\gamma})^N}{1 - e^{-i\gamma}} \\ &= \frac{e^{-i\gamma N/2} (e^{i\gamma N/2} - e^{-i\gamma N/2})}{e^{-i\gamma/2} (e^{i\gamma/2} - e^{-i\gamma/2})} \\ &= e^{-i\gamma(N-1)/2} \frac{\sin(\gamma N/2)}{\sin(\gamma/2)} \cdot \frac{1}{2i} \cdot \frac{2i}{1} \\ &= e^{-i\pi(N-1) \frac{\lambda x'}{\lambda l}} \frac{\sin\left(\frac{\pi N \lambda x'}{\lambda l}\right)}{\sin\left(\frac{\pi \lambda x'}{\lambda l}\right)} \end{aligned}$$

so

$$g(x', y') = a \operatorname{sinc}\left(a \frac{x'}{\lambda l}\right) e^{-i\pi(N-1) \frac{\lambda x'}{\lambda l}} \frac{\sin\left(\frac{\pi N \lambda x'}{\lambda l}\right)}{\sin\left(\frac{\pi \lambda x'}{\lambda l}\right)}$$

we observe intensity

$$|g(x', y')|^2 = a^2 \text{sinc}^2\left(\frac{ax'}{\lambda l}\right)$$

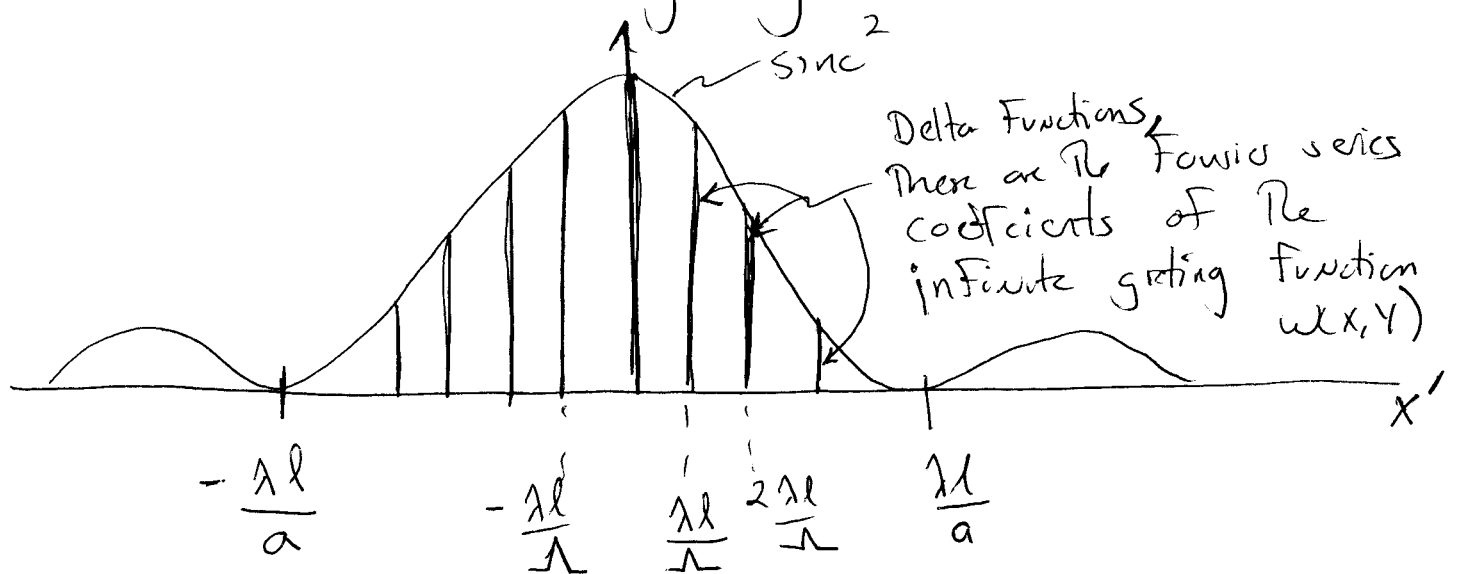
$$\frac{\sin^2\left(\frac{\pi N \lambda x'}{\lambda l}\right)}{\sin^2\left(\frac{\pi \lambda x'}{\lambda l}\right)}$$

when $N \rightarrow \infty$

This

goes to a delta function

so for an infinite grating:

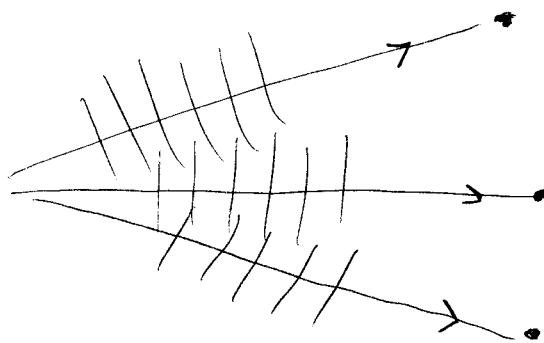
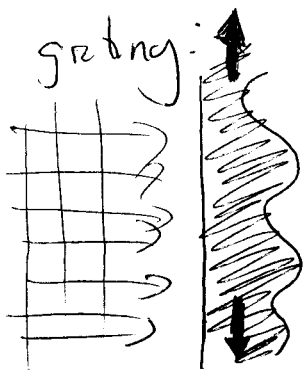


~~As an aside:~~

As an aside: The F.T. of $f(x) = \sin(\omega_0 x)$ is $\delta(f) + \delta(f - \omega_0) + \delta(f + \omega_0)$

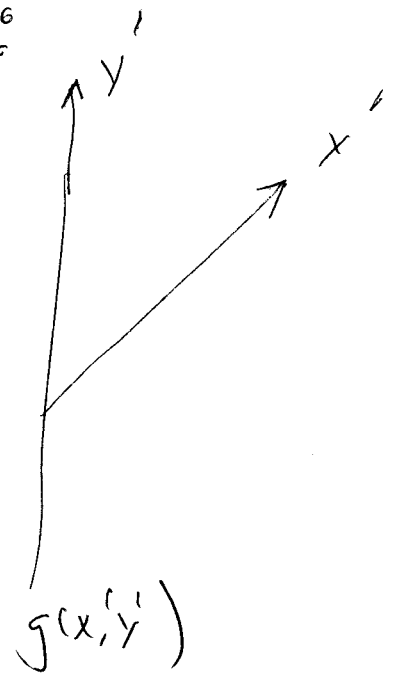
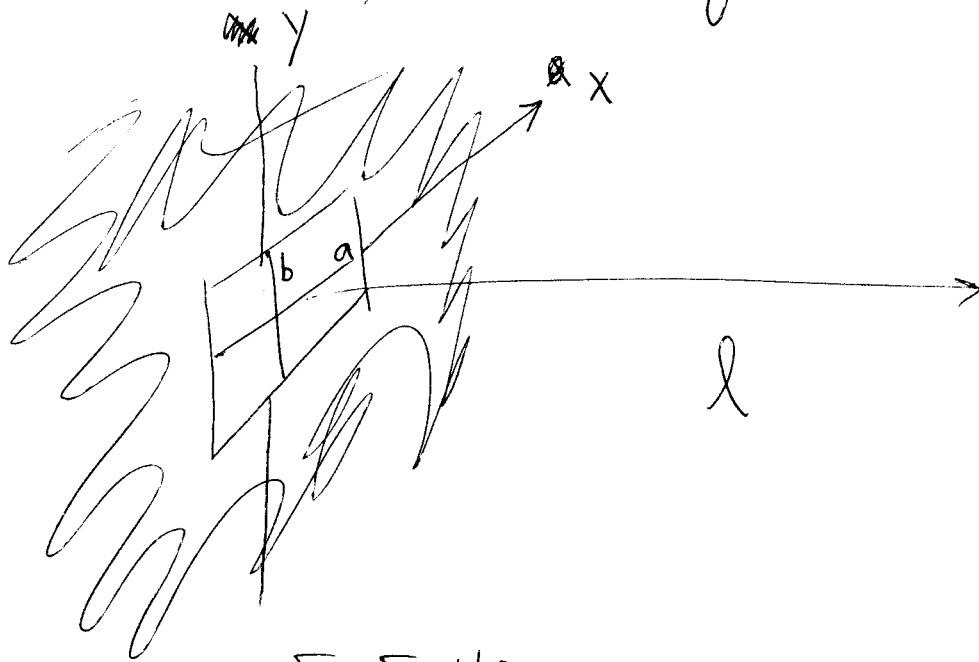
which is what we saw for an infinite sinusoidal!

grating:



so this is a general result for infinite gratings.

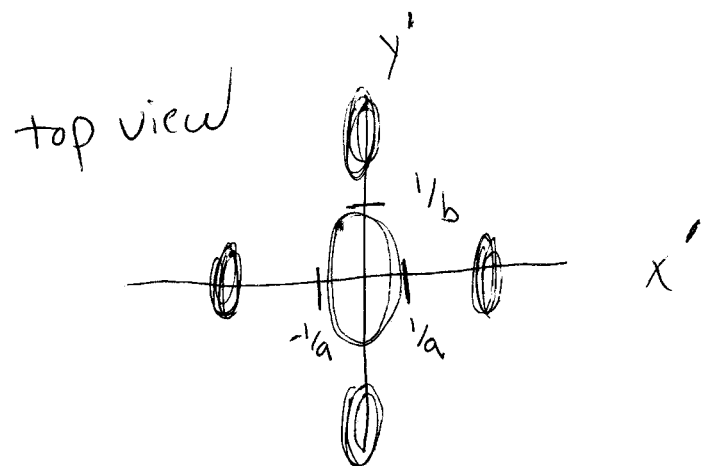
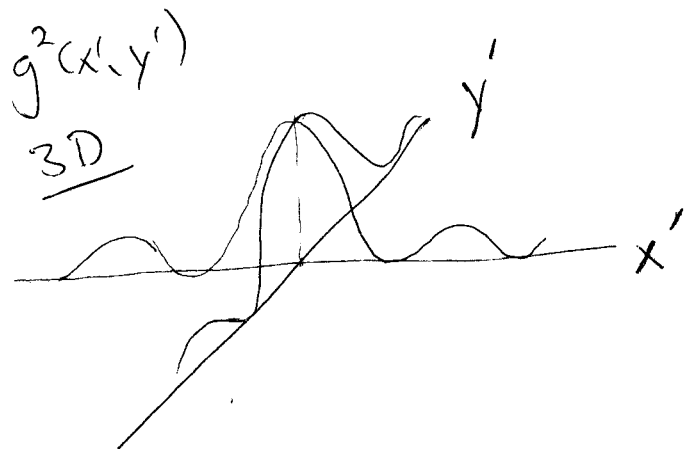
similarly for a square aperture:



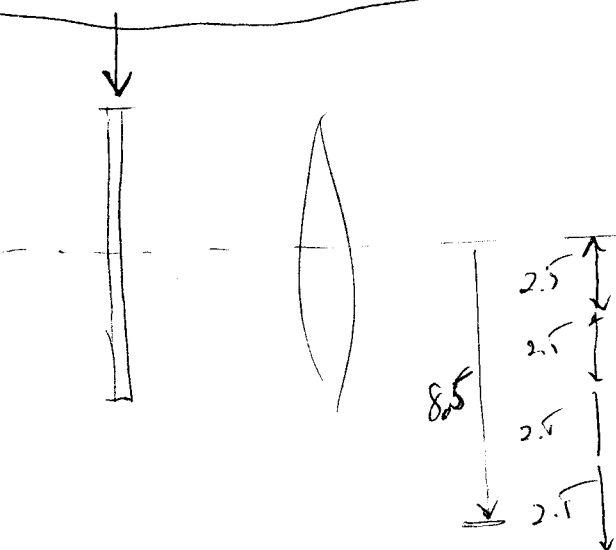
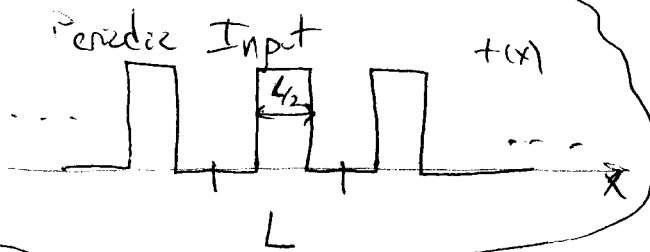
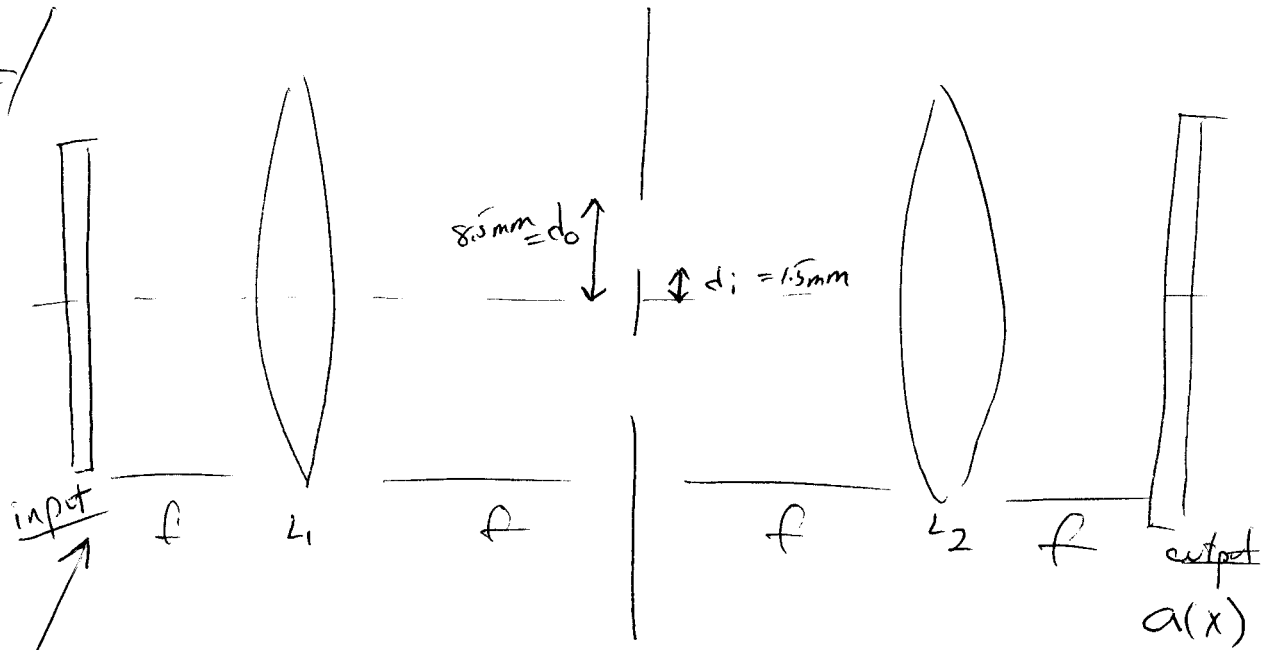
in Far Field:

$$g(x', y') = \text{F.T.}(W(x, y)) \Big|_{\substack{u = x'/\lambda l \\ v = y'/\lambda l}}$$

$$= ab \text{sinc}\left(a \frac{x'}{\lambda l}\right) \text{sinc}\left(b \frac{y'}{\lambda l}\right)$$



#2/



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~ diffracted order
weighed by
fourier series
coefficients

$$\frac{\lambda f}{L}$$

$$\frac{\lambda f}{L} = \frac{(5 \times 10^{-6}) (10 \times 10^{-2})}{20 \times 10^{-6}} = 2.5 \text{ mm}$$

mask allows order $\pm 1, \pm 2, \pm 3$ to pass.

so intuitively ^{in the output plane} we have eliminated DC & High Freq Terms

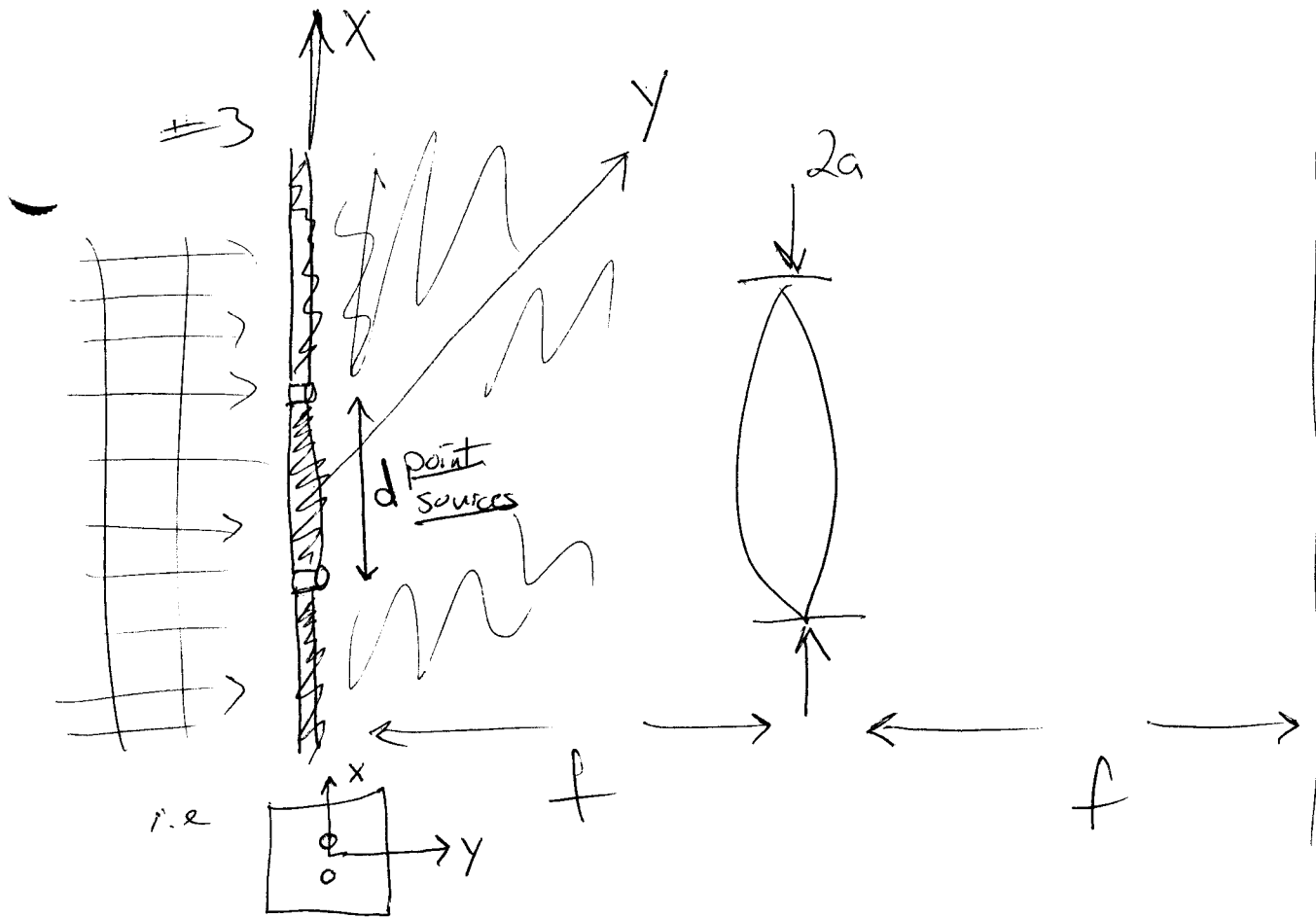
$$c_1 = 1/\pi = c_{-1}$$

$$c_2 = 0 = c_{-2}$$

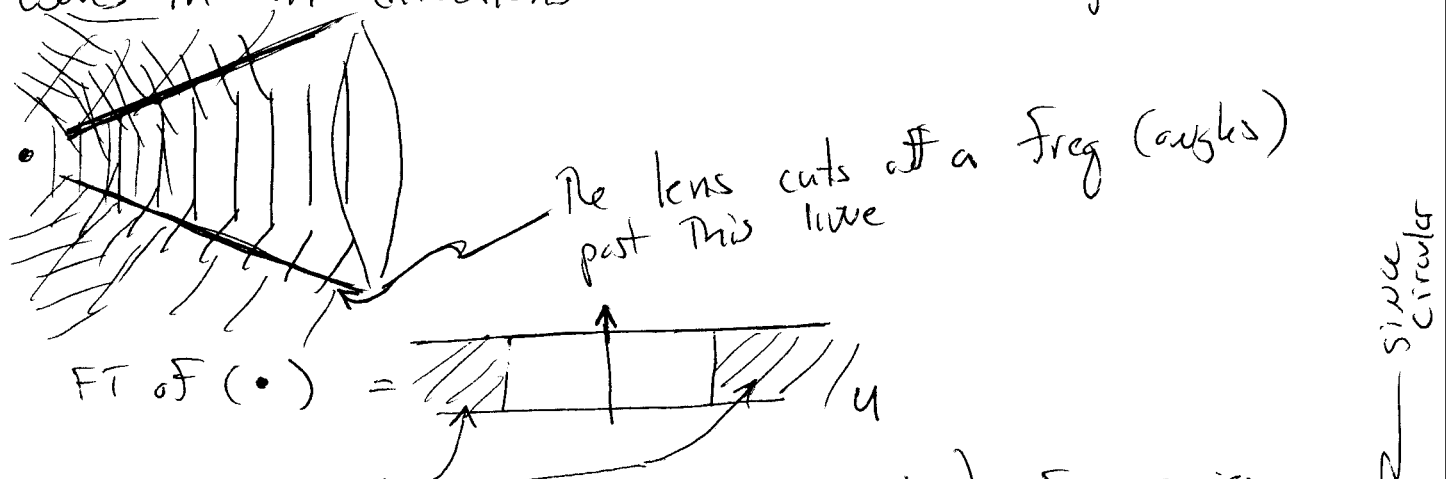
$$c_3 = -1/3\pi = c_{-3}$$

$$a(x) = \frac{1}{\pi} \left(e^{-i2\pi \frac{x'}{L}} + e^{i2\pi \frac{x'}{L}} \right) - \frac{1}{3\pi} \left(e^{-i2\pi \frac{3x'}{L}} + e^{i2\pi \frac{3x'}{L}} \right)$$

$$a(x) = \frac{2}{\pi} \left[\cos\left(2\pi \frac{x'}{L}\right) - \frac{1}{3} \cos\left(2\pi \frac{3x'}{L}\right) \right]$$



There are several equivalent ways to look at this. First imagine a single point source, it radiates plane waves in all directions (i.e. The FT of a point is all freq)



The aperture cuts off some of these high frequencies

at the image plane we get the Fourier Transform of what was passed i.e. FT of [rectangle] = [sinc wave]

we saw this in the last homework for a circular aperture

Another way is to say That For an imaging system
 The output Field is The input Field convolved
 with The lens / image system impulse response

i.e

$$g(x', y') = g(x, y) * h(x, y)$$

so for a single point & 1:1 image system
 (circular lens)

$$g(x', y') = \delta(x, y) * \frac{2J(\pi a \rho / \lambda f)}{\pi a \rho / \lambda f} \quad \text{where } \rho = (x^2 + y^2)^{1/2}$$

$$= \frac{2J(\pi a \rho / \lambda f)}{\pi a \rho / \lambda f}$$

← "jinc"

since only interested along x' axis
 $y' = 0$

$$= \frac{2J(\pi a x / \lambda f)}{\pi a x / \lambda f}$$

now for two point sources :

$$g(x', y') = \left[\delta(x - d/2) + \delta(x + d/2) \right] * \frac{2J(\pi a x / \lambda f)}{\pi a x / \lambda f}$$

$$g(x', y') = \frac{2J\left(\frac{\pi a}{\lambda f} (x - d/2)\right)}{\frac{\pi a}{\lambda f} (x - d/2)} + \frac{2J\left(\frac{\pi a}{\lambda f} (x + d/2)\right)}{\frac{\pi a}{\lambda f} (x + d/2)}$$

- The previous was for a coherent source

$$\text{Intensity}(x, y) = |\text{field}(x, y)|^2$$

- for incoherent

$$\text{Intensity}(x, y) = |\text{"field" in}|^2 * |\text{system impulse}|^2$$

so

$$I(x', y')_{\text{coherent}} = \left[\frac{2J\left(\frac{\pi a}{\lambda f}(x' - d/2)\right)}{\frac{\pi a}{\lambda f}(x' - d/2)} + \frac{2J\left(\frac{\pi a}{\lambda f}(x' + d/2)\right)}{\frac{\pi a}{\lambda f}(x' + d/2)} \right]^2$$

~~where~~
we are interested in

$$d = 3.55 \frac{\lambda f}{a} \quad 1.22 \frac{\lambda f}{a} \quad 0.41 \frac{\lambda f}{a}$$

so in normalized coordinates

$$I(x', y')_{\text{coherent}} = \left[\frac{2J(\pi(\bar{x} - \bar{d}/2))}{\bar{x} - \bar{d}/2} + \frac{2J(\pi(\bar{x} + \bar{d}/2))}{\bar{x} + \bar{d}/2} \right]^2$$

$$\text{w/ } \bar{d} = 3.55, 1.22, 0.41$$

and for incoherent:

$$I(x', y')_{\text{incoherent}} = \left[\frac{2J(\pi(\bar{x} - \bar{d}/2))}{\bar{x} - \bar{d}/2} \right]^2 + \left[\frac{2J(\pi(\bar{x} + \bar{d}/2))}{\bar{x} + \bar{d}/2} \right]^2$$

see following plots.

```

%problem set #4
%problem # 3
%2 point resolution
%Brian Anthony

x = -5:.01:5;

sep = 3.55
%sep = 1.22
%sep = .41

g1 = 2*besselj(1,pi*(x+sep/2))./(pi*(x+sep/2));
g2 = 2*besselj(1,pi*(x-sep/2))./(pi*(x-sep/2));
goutC = (g1 + g2).^2;
goutI = (g1.^2 + g2.^2);

figure(1)
subplot 411
plot(x,g1)
title('g1')

subplot 412
plot(x,g2)
title('g2')

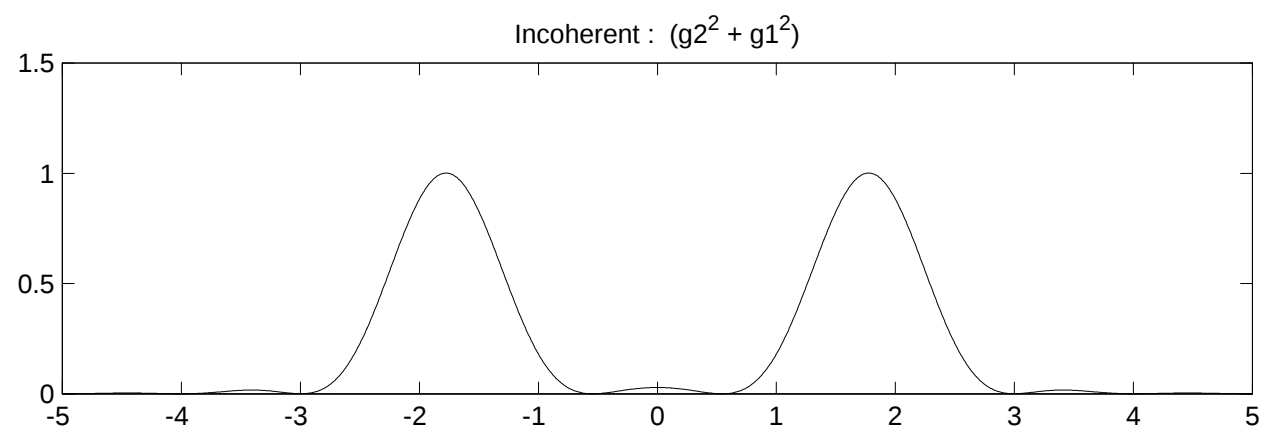
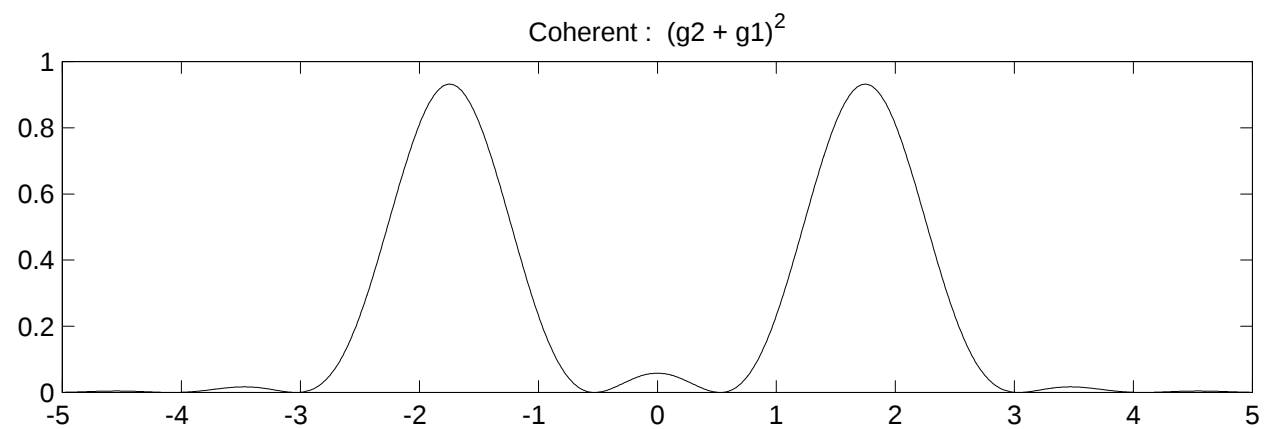
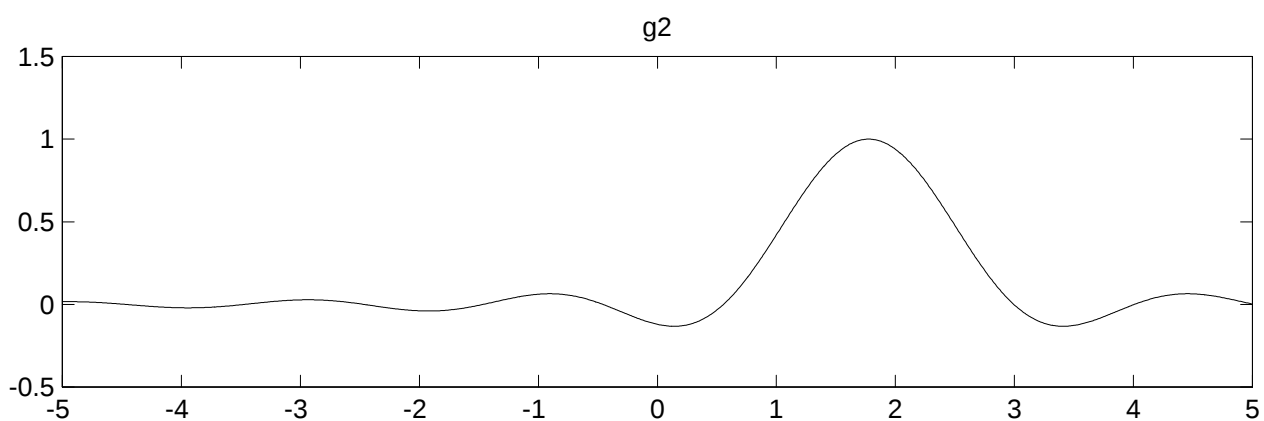
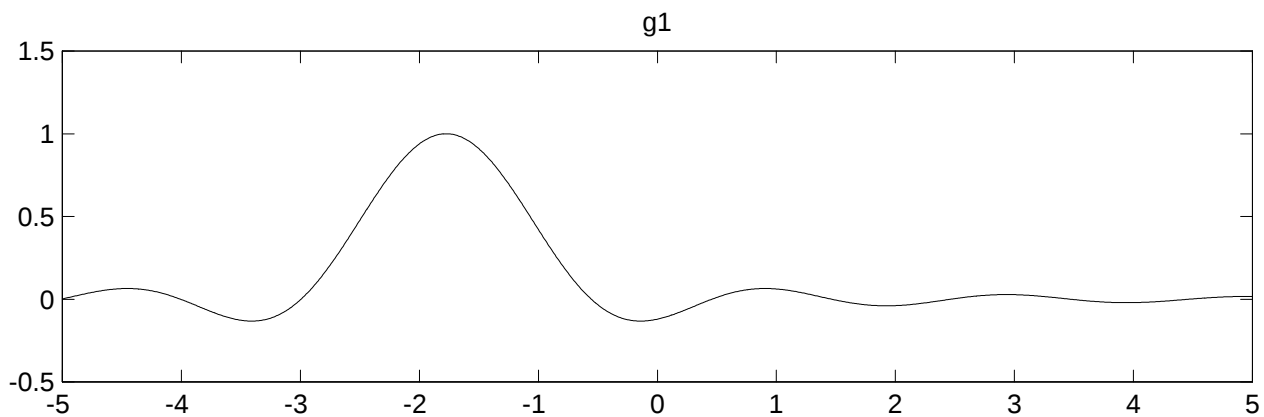
subplot 413
plot(x,goutC)
title('Coherent : (g2 + g1)^2')
zoom on

subplot 414
plot(x,goutI)
title('Incoherent : (g2^2 + g1^2)')
zoom on

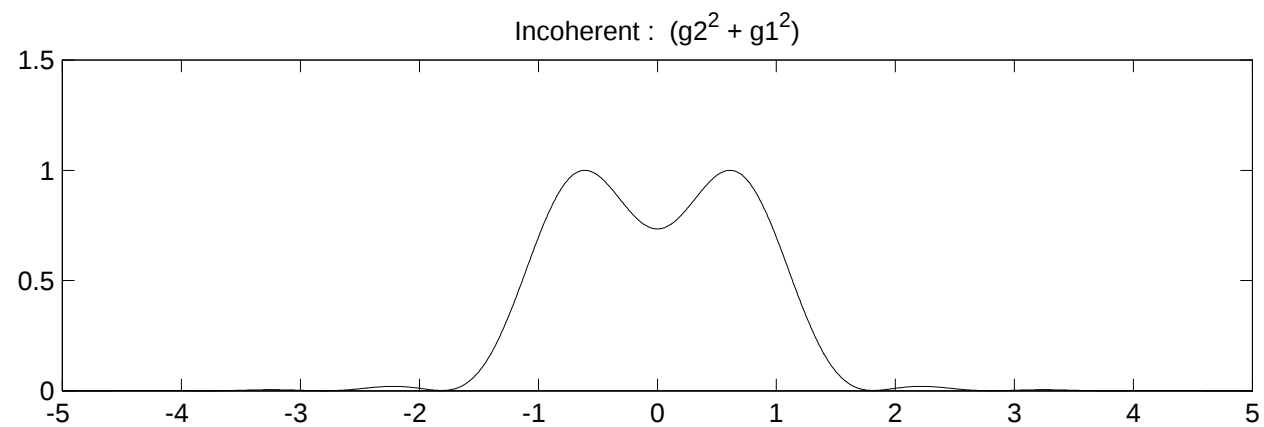
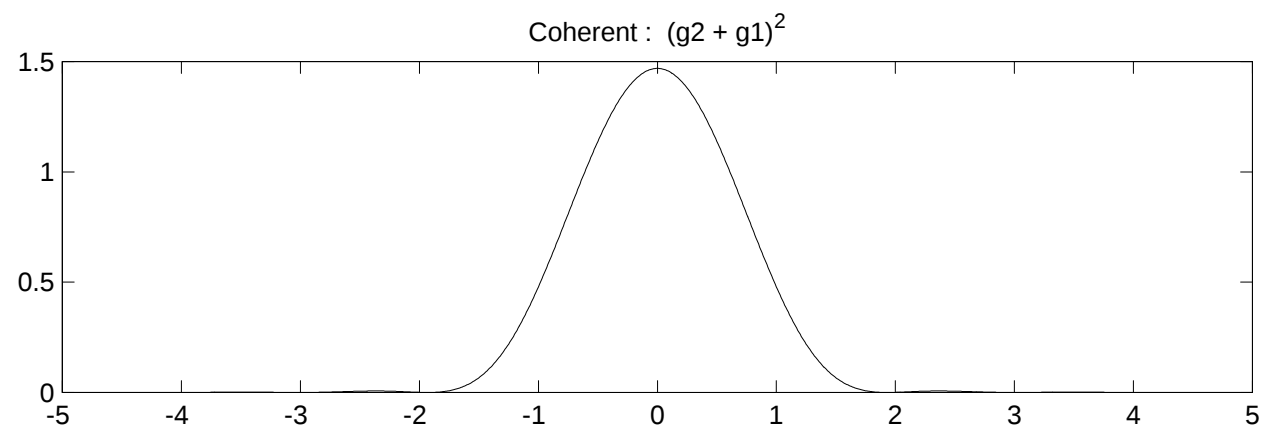
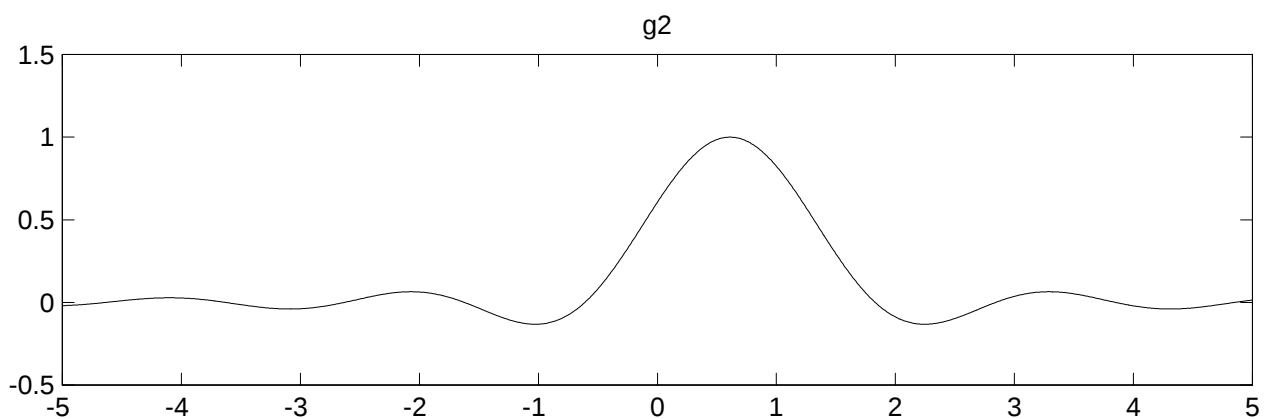
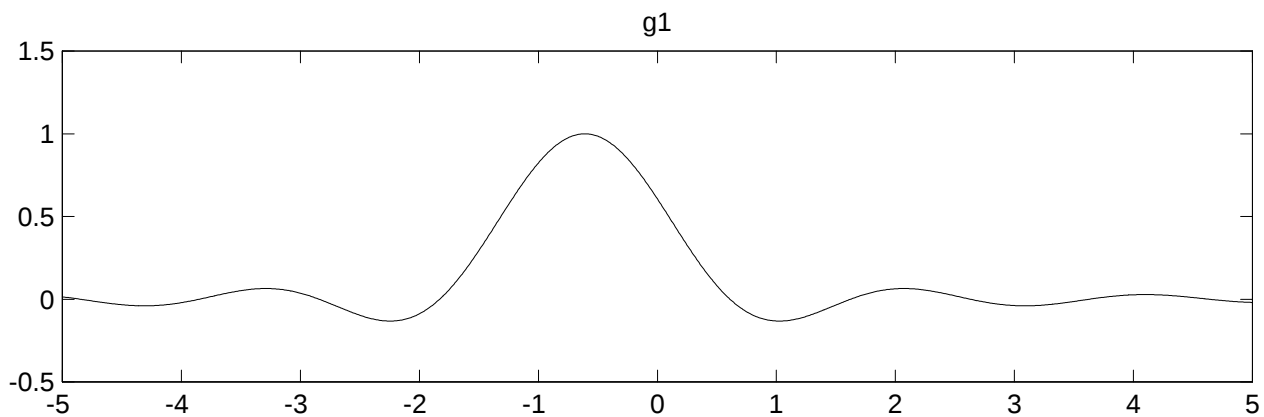
str = ['Normalized image coordinates. Separation = ' num2str(sep) '*lam*a/f'];

xlabel(str)

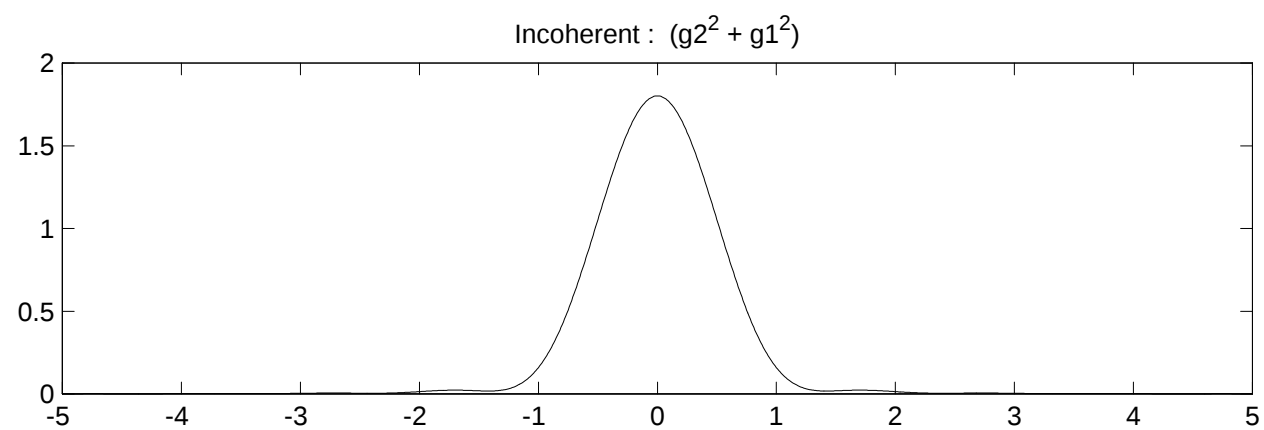
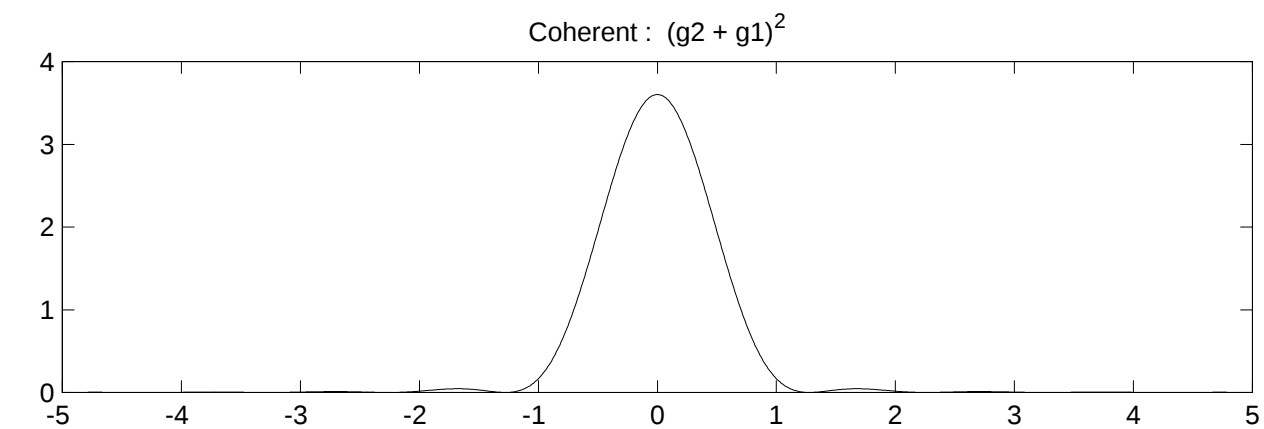
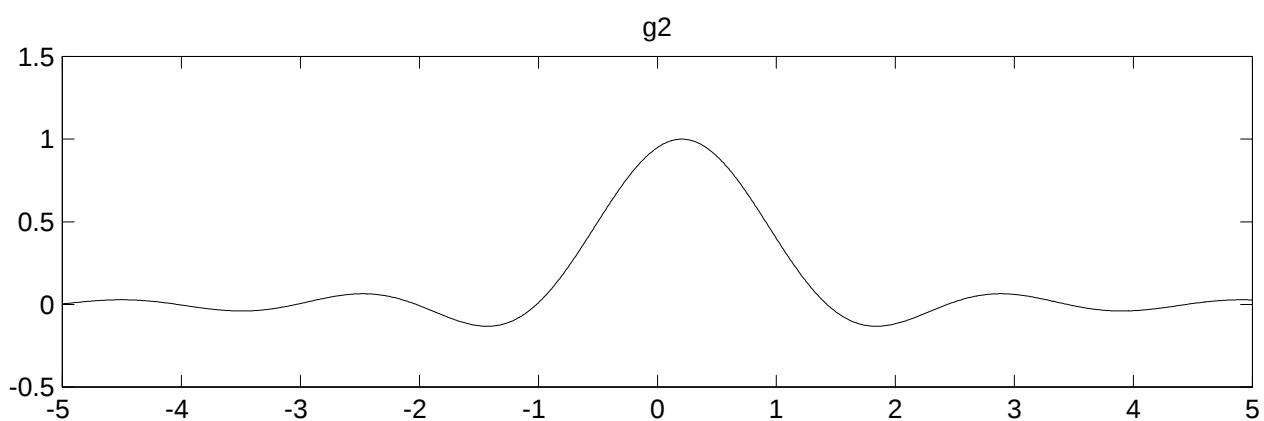
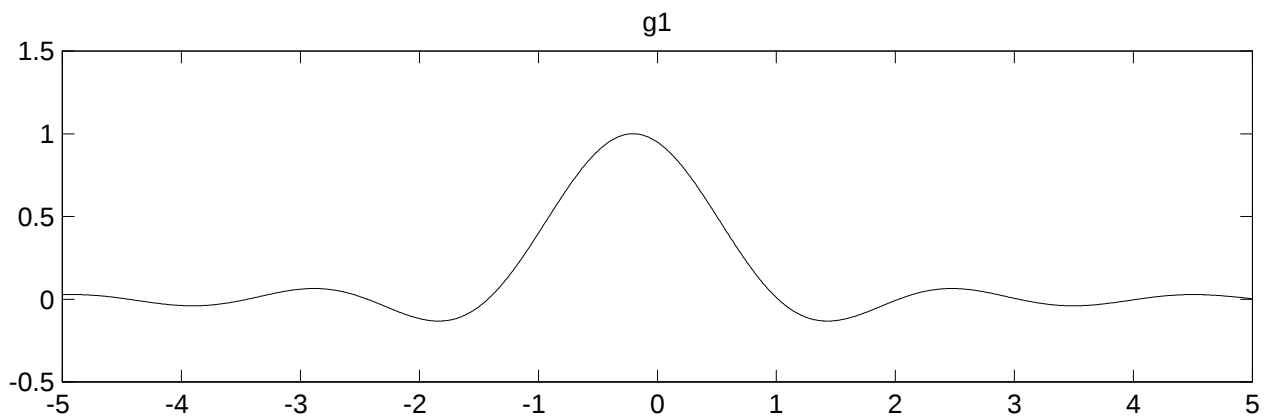
```



Normalized image coordinates. Separation = $3.55 \cdot \lambda \cdot a / f$



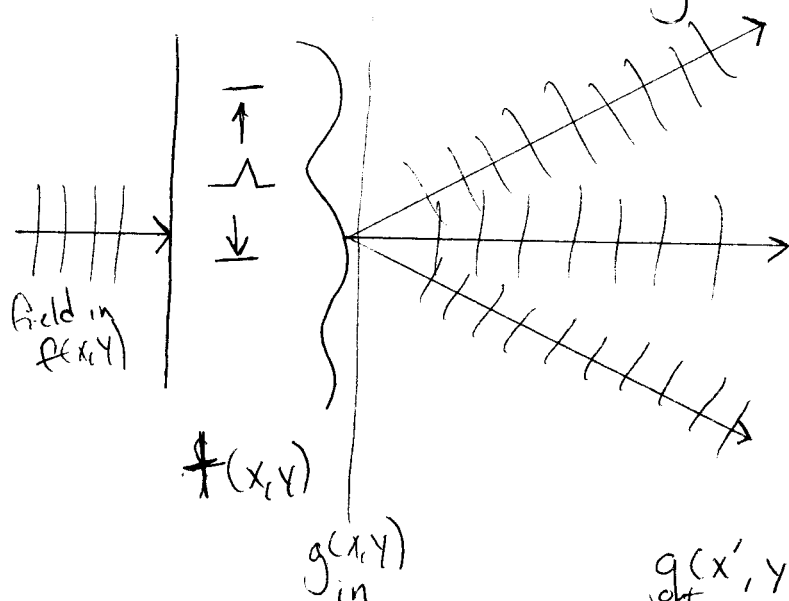
Normalized image coordinates. Separation = $1.22 \cdot \lambda \cdot a / f$



Normalized image coordinates. Separation = $0.41 \cdot \lambda \cdot a / f$

#4

First,

what does a ^{sine} grating do??

3 diffracted orders.

at Far Field ($\rightarrow \infty$)

$$g(x', y') = \text{FT}(\underbrace{t(x, y)}_{\text{sine grating}} \times \underbrace{f_{\text{in}}(x, y)}_{\text{plane wave}})_{g_{\text{in}}}$$

if f_{in} is a plane wave = 1
 $t(x, y)$ sine grating

$$= \underbrace{\delta(u, v) + \delta(u - \frac{1}{\lambda}) + \delta(u + \frac{1}{\lambda})}_{\text{"I" "II" "III"}}$$

where $u = x' / \lambda l$

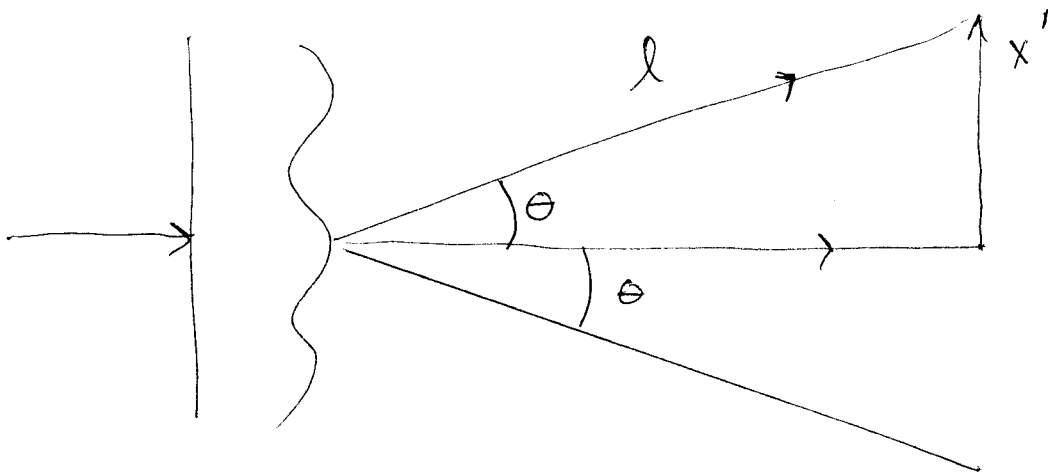
The point at infinity is at what angle?

well it occurs where $u = \frac{1}{\lambda}$ or $\frac{x'}{\lambda l} = \frac{1}{\lambda}$

$$\frac{x'}{l} = \frac{1}{\lambda}$$

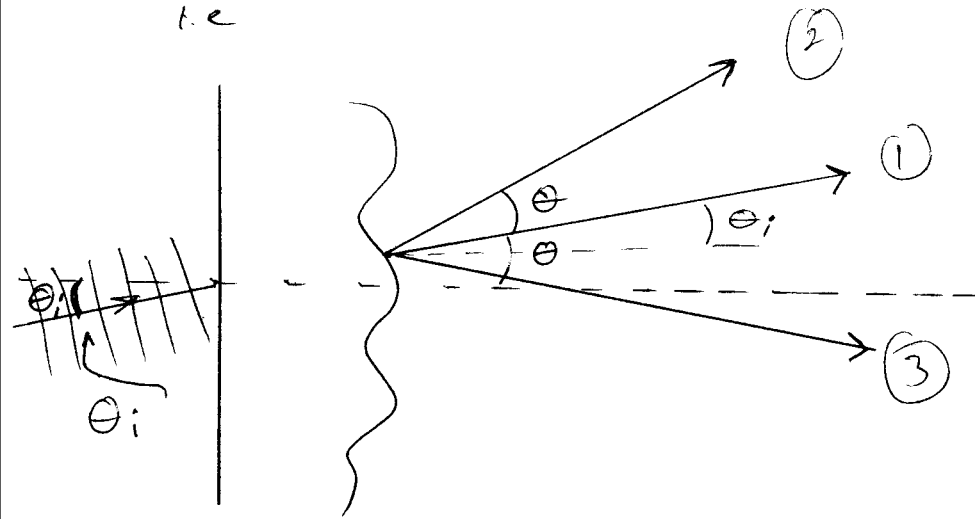
or in other words

$$\sin \theta = \frac{x'}{l} = \frac{1}{\lambda}$$



so you can imagine ^(intuitively I hope) That tilting the input plane wave tilts the outputs

i.e



in Fourier domain

$$g_{out}(x', y') = FT(f(x, y) \cdot f_{in}(x, y))$$

$$= FT(\text{sine grating} \times e^{i 2\pi \sin \theta_i / \lambda x})$$

$$= \underbrace{\delta(u - \frac{\sin \theta_i}{\lambda})}_{(1)} + \underbrace{\delta(u - \frac{1}{\lambda} - \frac{\sin \theta_i}{\lambda})}_{(2)} + \underbrace{\delta(u + \frac{1}{\lambda} - \frac{\sin \theta_i}{\lambda})}_{(3)}$$

so the angles are given:

~~scribbles~~ ① $\frac{\sin \theta_1}{\lambda} = \frac{\sin \theta_i}{\lambda} \Rightarrow \theta_1 \approx \theta_i$ in paraxial

② $\frac{\sin \theta_2}{\lambda} = \frac{1}{\lambda} + \frac{\sin \theta_i}{\lambda} \Rightarrow \theta_2 = \frac{\lambda}{\lambda} + \theta_i$

③ $\frac{\sin \theta_3}{\lambda} = -\frac{1}{\lambda} + \frac{\sin \theta_i}{\lambda} \Rightarrow \theta_3 = -\frac{\lambda}{\lambda} + \theta_i$

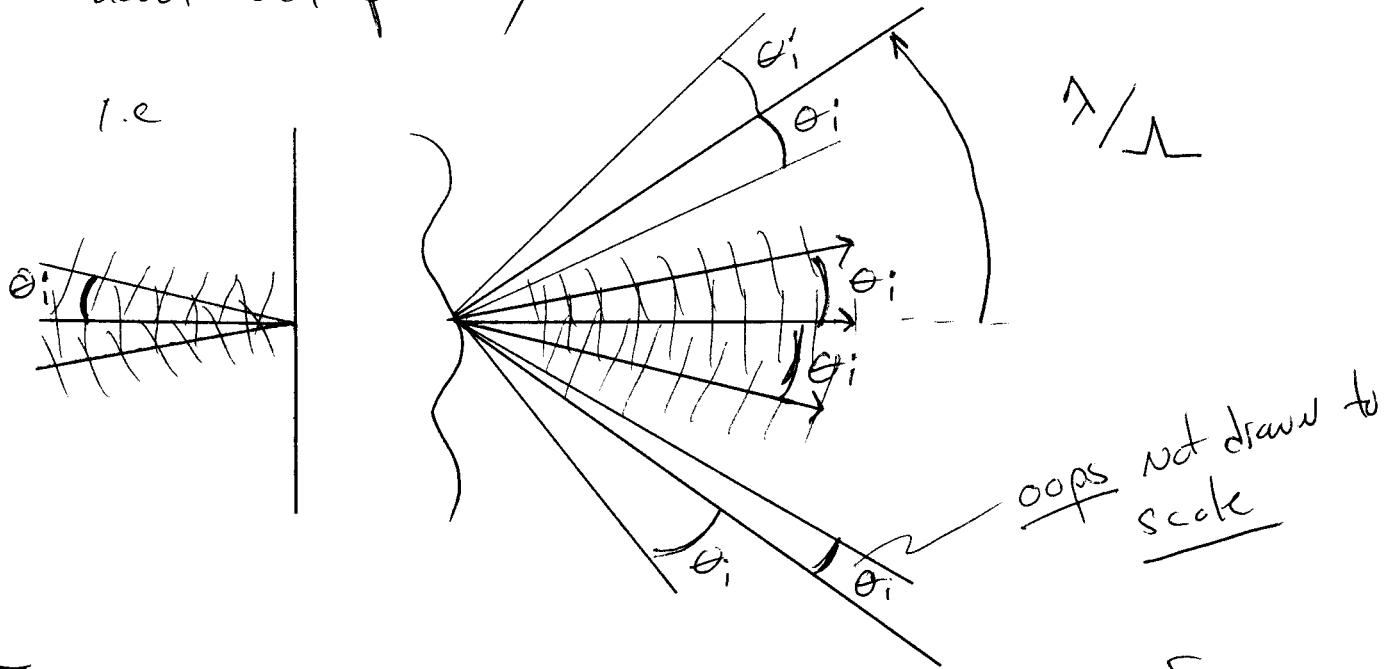
multiplication in space = convolution in Freq

or modulation in space = shift in Freq

remember $u = x'/\lambda d$
 $= \frac{\sin \theta}{\lambda}$

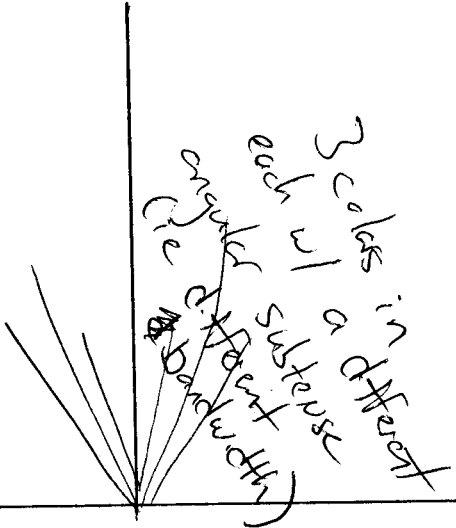
so what does this mean?

IF a ^{single} grating has a cone (limited angular subtense) coming in it will have a similar cone at the output about each primary direction. (diffracted order)



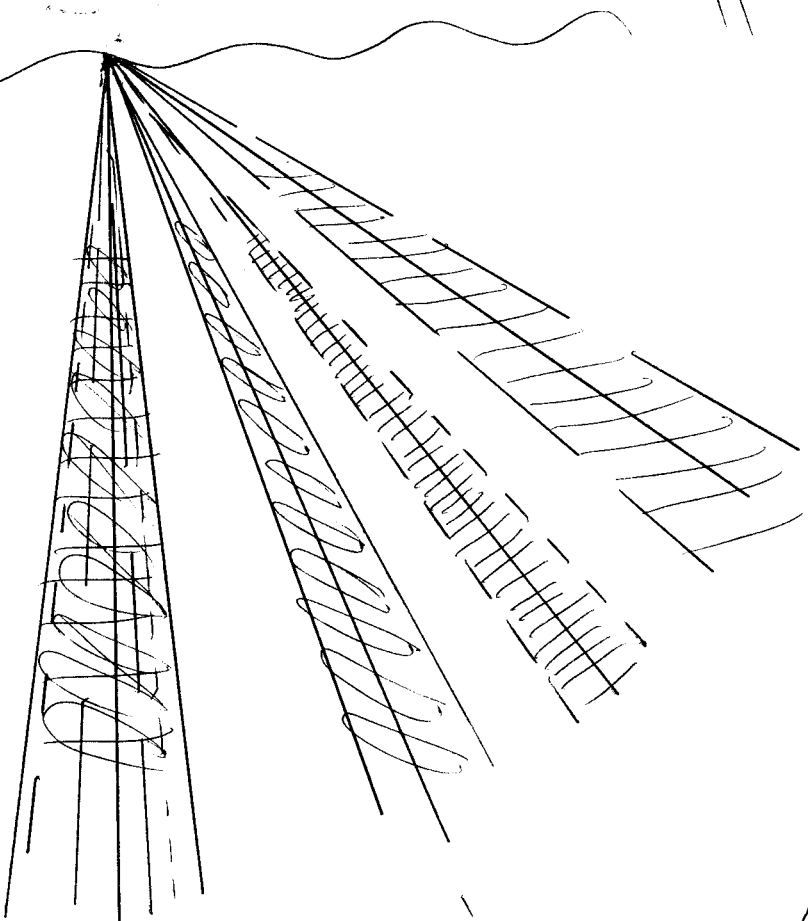
so we see that if we have ^{cones of} multiple colors coming into the grating (each with different λ) they will all travel down the optical axis and then off at angles that depend on their λ so what we are trying to achieve is this:

The idea of the problem



Input
3 colors in, each with a different range of phase waves (angular subcase) (or bandwidth)

Note
$$u_0 = \frac{1}{\lambda}$$



Separation out.

- each range of angles in for each of the 3 colors is centered about its 3 diffraction orders
- and we want to separate them by making sure that the 3 Blue and green (angular subcases of phase waves) and 3 Red are such that the output bundles don't overlap

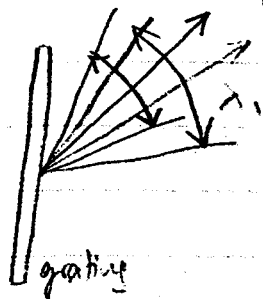
$$\frac{n_1}{\lambda}$$

$$\frac{n_2}{\lambda}$$

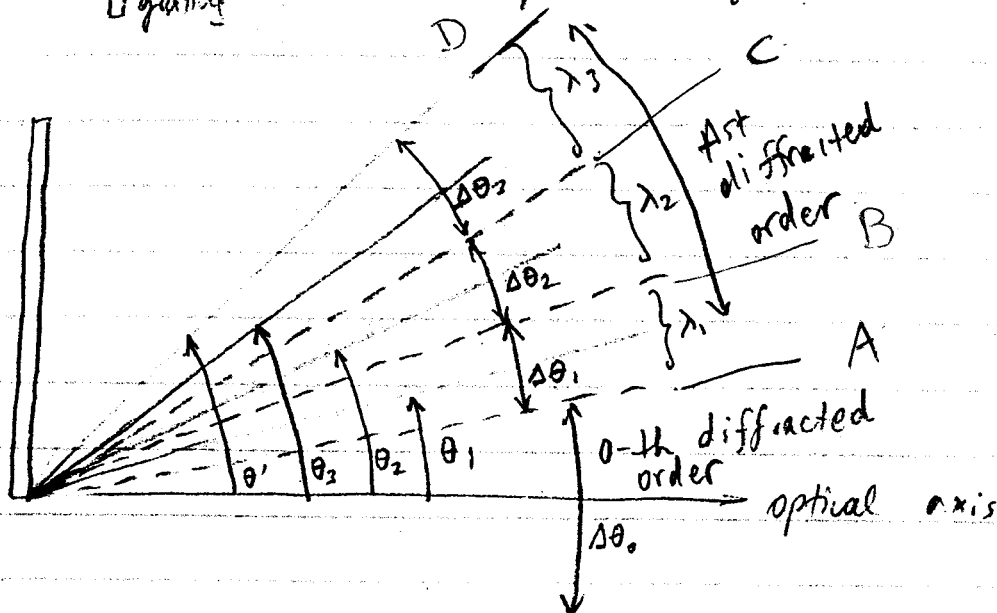
$$\frac{n_3}{\lambda}$$

(2) a) Broad-band input:

#4



cannot be separated
 $\therefore$ spatial spectra must fit within the angle acceptance ranges of lenses L_1, L_2, L_3 , respectively



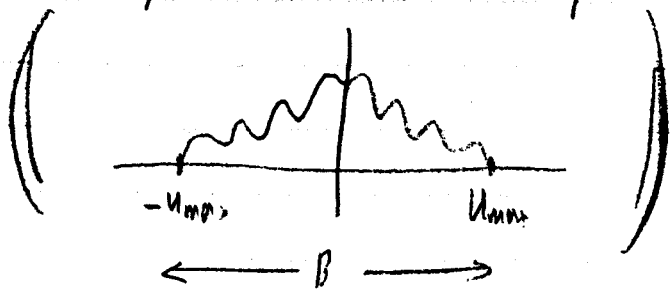
Angular spread of j -th order ($j=1,2,3$) $\Delta\theta_j = \lambda_j B_j$

0-th order contains all colors $\Rightarrow$ angular spread $\Delta\theta_0 = \max \{ \lambda_j B_j \}$

constraints:

$$\begin{cases} A: \theta_1 - \frac{\Delta\theta_1}{2} > \frac{\Delta\theta_0}{2} \Rightarrow \lambda_1 u_0 - \frac{\lambda_1 B_1}{2} \geq \frac{1}{2} \max \{ \lambda_j B_j \} & (1) \\ B: \theta_2 - \frac{\Delta\theta_2}{2} > \theta_1 + \frac{\Delta\theta_1}{2} \Rightarrow \lambda_2 u_0 - \frac{\lambda_2 B_2}{2} \geq \lambda_1 u_0 + \frac{\lambda_1 B_1}{2} & (2) \\ C: \theta_3 - \frac{\Delta\theta_3}{2} > \theta_2 + \frac{\Delta\theta_2}{2} \Rightarrow \lambda_3 u_0 - \frac{\lambda_3 B_3}{2} \geq \lambda_2 u_0 + \frac{\lambda_2 B_2}{2} & (3) \\ D: \theta_3 + \frac{\Delta\theta_3}{2} < \theta' \Rightarrow \lambda_3 u_0 + \frac{\lambda_3 B_3}{2} \geq \frac{1}{2} & (4) \end{cases}$$

b) SLM pixel size $b =$, max possible frequency $= \frac{1}{2b} \Rightarrow B_1 = B_2 = B_3 = \frac{1}{b}$



Substitute into (1) & (4) using

$$B_1 = B_3 = \frac{1}{b} \quad \lambda_1 = \lambda \quad \lambda_3 = 3\lambda$$

7) b) cont'd

$$(1) \Rightarrow \lambda u_0 - \frac{\lambda}{2b} = \frac{1}{2} \cdot \left(3\lambda \cdot \frac{1}{b} \right) \Rightarrow u_0 = \frac{2}{b}$$

← max since $\frac{\lambda}{b} < \frac{\lambda_2}{b} < \frac{3\lambda}{b}$
 equality ensures orders 0th and 1st @ λ_1 are adjacent
 $\Rightarrow \theta_1$ is as small as possible

$$(4) \Rightarrow 3\lambda u_0 + \frac{3\lambda}{2b} = \frac{1}{2} \Rightarrow \frac{15\lambda}{2b} = \frac{1}{2} \Rightarrow b = 15\lambda, u_0 = \frac{2}{15\lambda}$$

← equality ensures highest spatial frequency component of order 1st @ λ_3 just misses the θ' constraint

c) Substitute into (2) & (3)

$$(2) \Rightarrow \lambda_2 \cdot \frac{2}{15\lambda} - \frac{\lambda_2}{30\lambda} \geq \frac{2\lambda}{15\lambda} + \frac{\lambda}{30\lambda} \Rightarrow \lambda_2 \geq \frac{\frac{2}{15} + \frac{1}{30}}{\frac{2}{15} - \frac{1}{30}} \lambda = \frac{5}{3} \lambda$$

$$(3) \Rightarrow 3\lambda \cdot \frac{2}{15\lambda} - \frac{3\lambda}{30\lambda} \geq \frac{\lambda_2}{5\lambda} + \frac{\lambda_2}{30\lambda} \Rightarrow \lambda_2 \leq 3 \frac{\frac{2}{15} - \frac{1}{20}}{\frac{2}{15} + \frac{1}{30}} \lambda = \frac{9}{5} \lambda$$

$$\lambda_1 = \lambda$$

$$1.67\lambda \leq \lambda_2 \leq 1.8\lambda \quad \leftarrow \text{allowable range for } \lambda_2.$$

$$\lambda_3 = 3\lambda$$

d) Sharp edges $\Rightarrow B_{1,2,3} = \infty$ because e.g. rect $\rightarrow$ sinc with freq. components extending all over to infinity. So colors mix.

BUT

